

# Effect of Supporter Material on Heat Evolution from Ni-based Nano-Composite Samples under Exposure to Hydrogen Isotope Gas

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# Oct. 2015, Collaborative Research Project

launched by six research institutes; Technova Inc., Tohoku Univ., Nissan Motor Co. Ltd., Nagoya Univ., Kobe Univ., Kyushu Univ.

## “Analysis and control of novel heat-reaction between metal-nanoparticles and hydrogen”

Objective:

- to verify the presence of the anomalous heat effect (**AHE**) generation phenomena
- to find guiding principles of power control
- to extend research activity as a national project, etc.

High-precision flow calorimetry systems;

one installed at Kobe U., Jun. 2013,

and new similar one installed at Tohoku U, Apr. 2016.

2016~2017, collaborative exam. at Kobe

using 4 kinds of samples

# Collaborative experiments done at Kobe-U, 2016~2017

(a)  $\text{Pd}_{0.044}\text{Ni}_{0.31}\text{Zr}_{0.65}$  ; PNZ3, PNZ4, PNZ5

(b)  $\text{Cu}_{0.044}\text{Ni}_{0.31}\text{Zr}_{0.65}$  ; CNZ5

- Amorphous mixture of Pd (or Cu), Ni & Zr by melt-spinning method  
⇒ Calcination at 450 °C for 100~60 h  
⇒ Formation of binary nanocomposite of Pd·Ni (or Cu·Ni) in  $\text{ZrO}_2$
- Oct. 2016, at ICCF20 (*J. Cond. Matter Nucl. Phys.*)

(c)  $\text{Cu}_{0.008}\text{Ni}_{0.079}$  supported by **mesoporous silica** (mp-S); CNS3

- $\text{NH}_3\text{aq}$  solution of  $\text{PdCl}_2$  &  $\text{NiCl}_2$  with mp-S suspended  
⇒ binary nanocomposite of Cu·Ni adsorbed on the pore surfaces

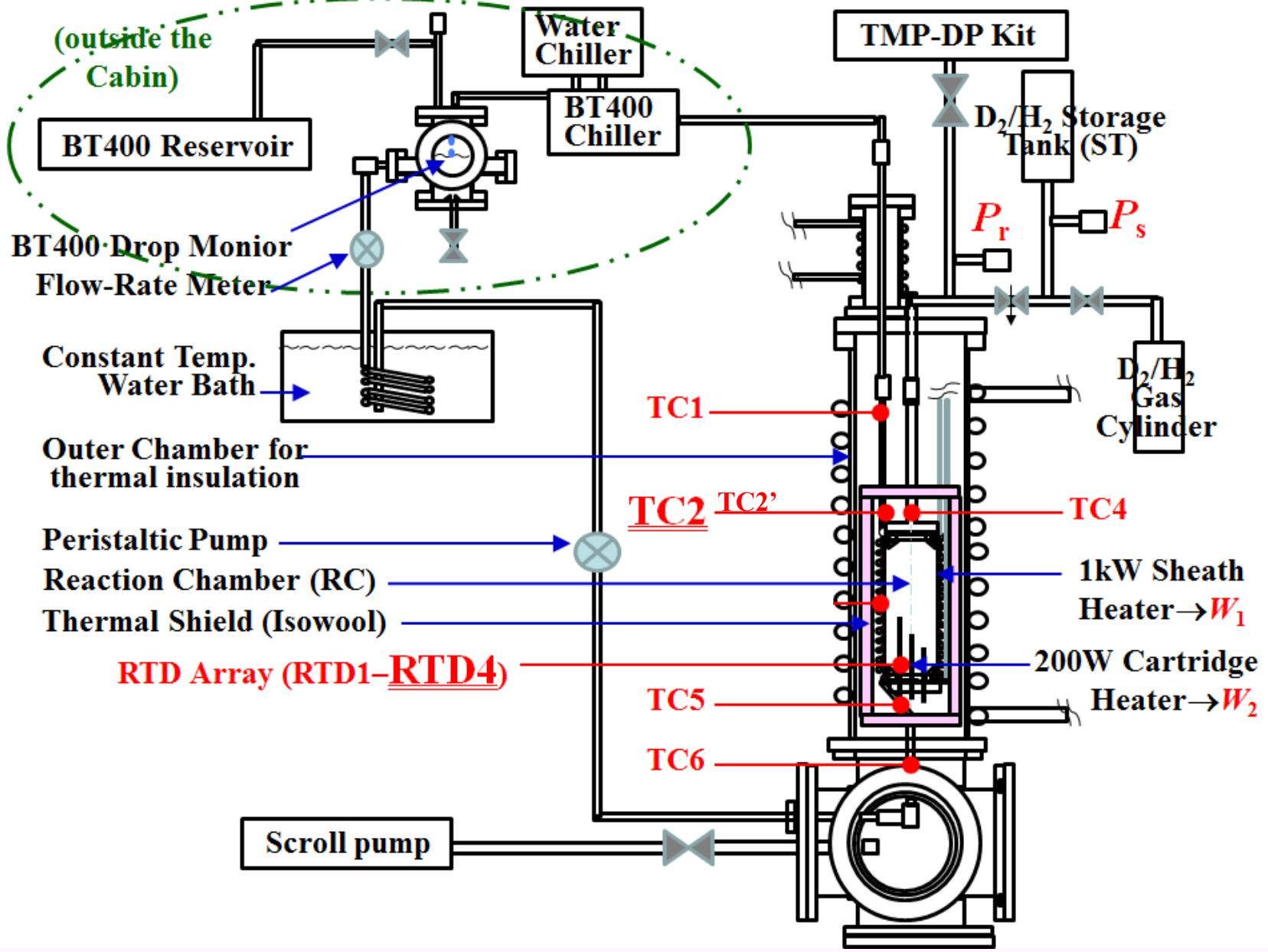
(d) Pd nanoparticles embedded in mesoscopic  $\text{SiO}_2$ ; PSf1

- Developed at Kyushu Univ.
- Mar. 2017, at JCF17 (*Proc. JCF17*)

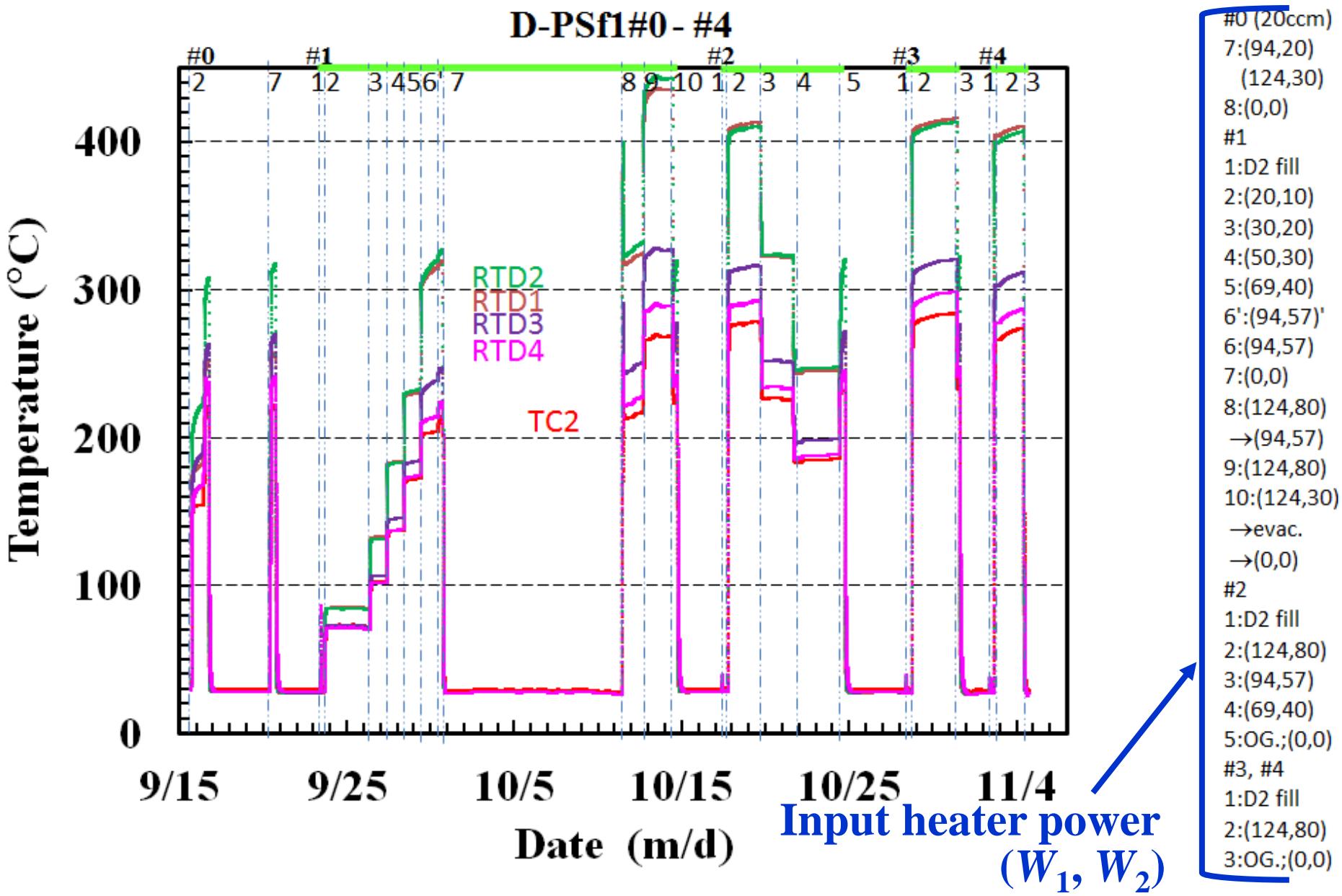
## Results

- Excess power at elevated temperatures around 300 °C observed only for binary-metal nanoparticle samples
- Excess power of 3 ~ 10 W lasting for a few weeks at elevated temperatures 200 ~ 300 °C, to result in integrated heat-energy of 20 MJ/mol-Ni, or 90 MJ/mol-H
- Unexplainable by any known chemical reaction

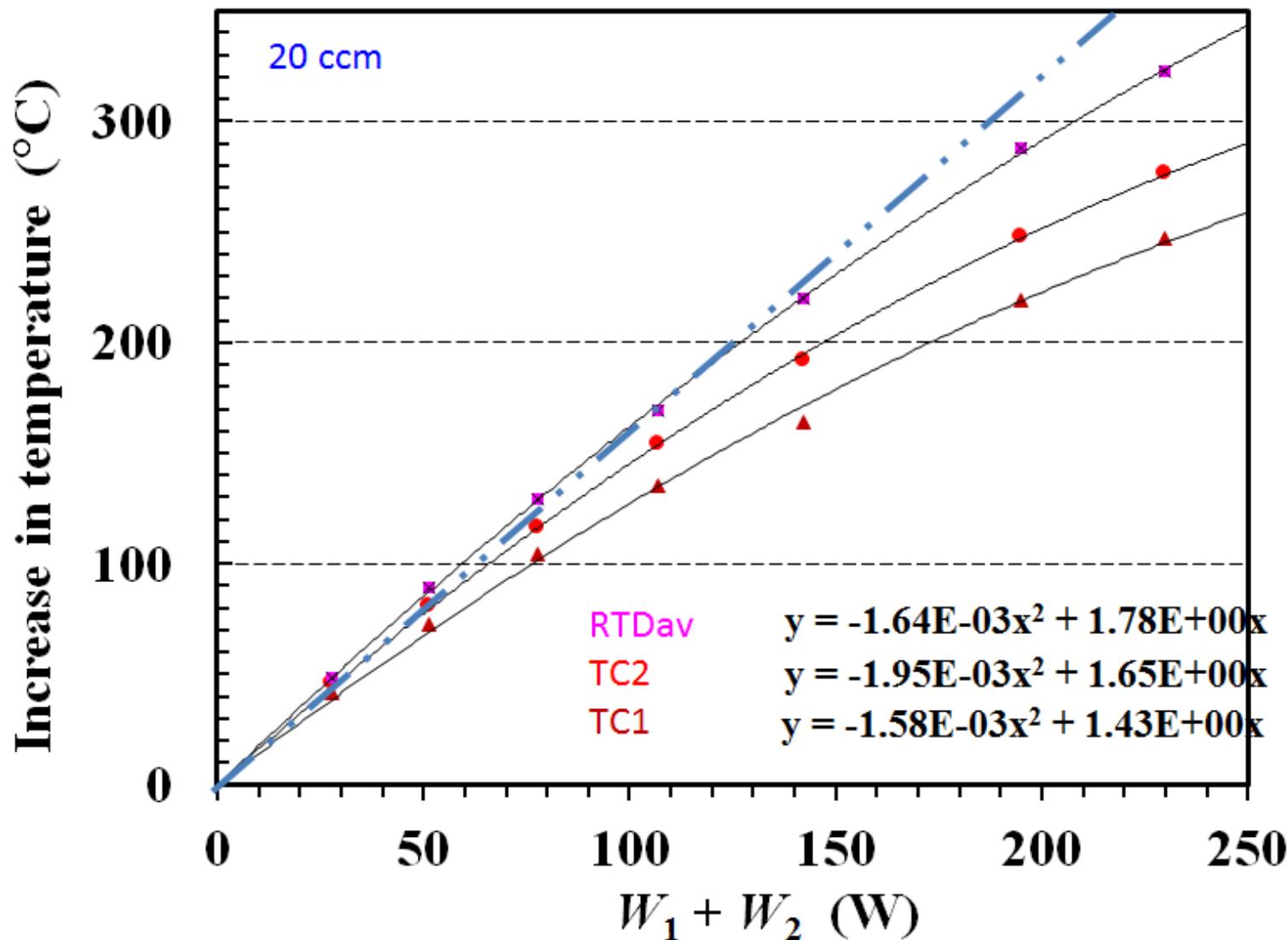
# High-precision evaluation equipment for anomalous heat effect



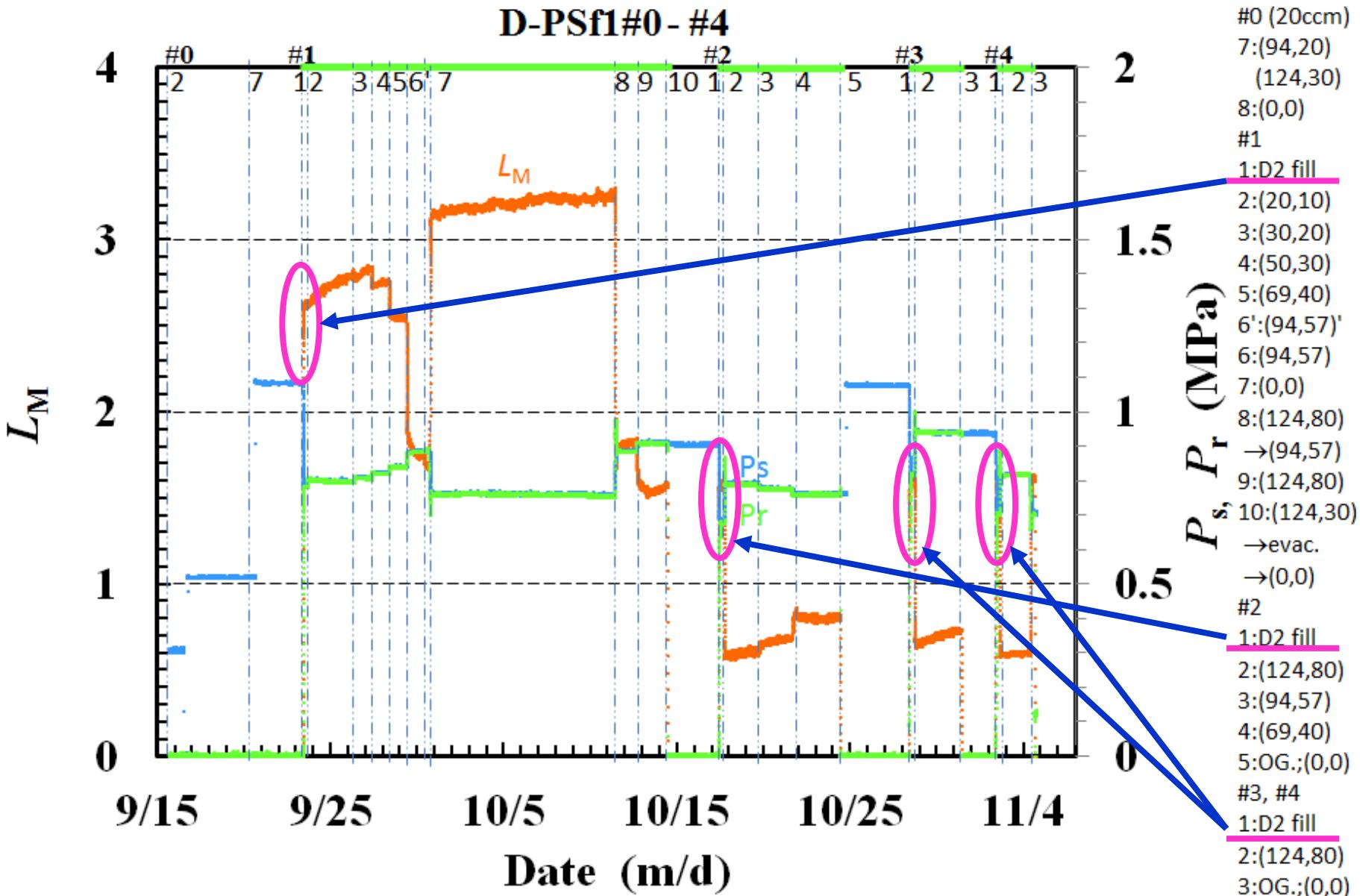
# Temperature history in D-PSf1#1 through #4 runs



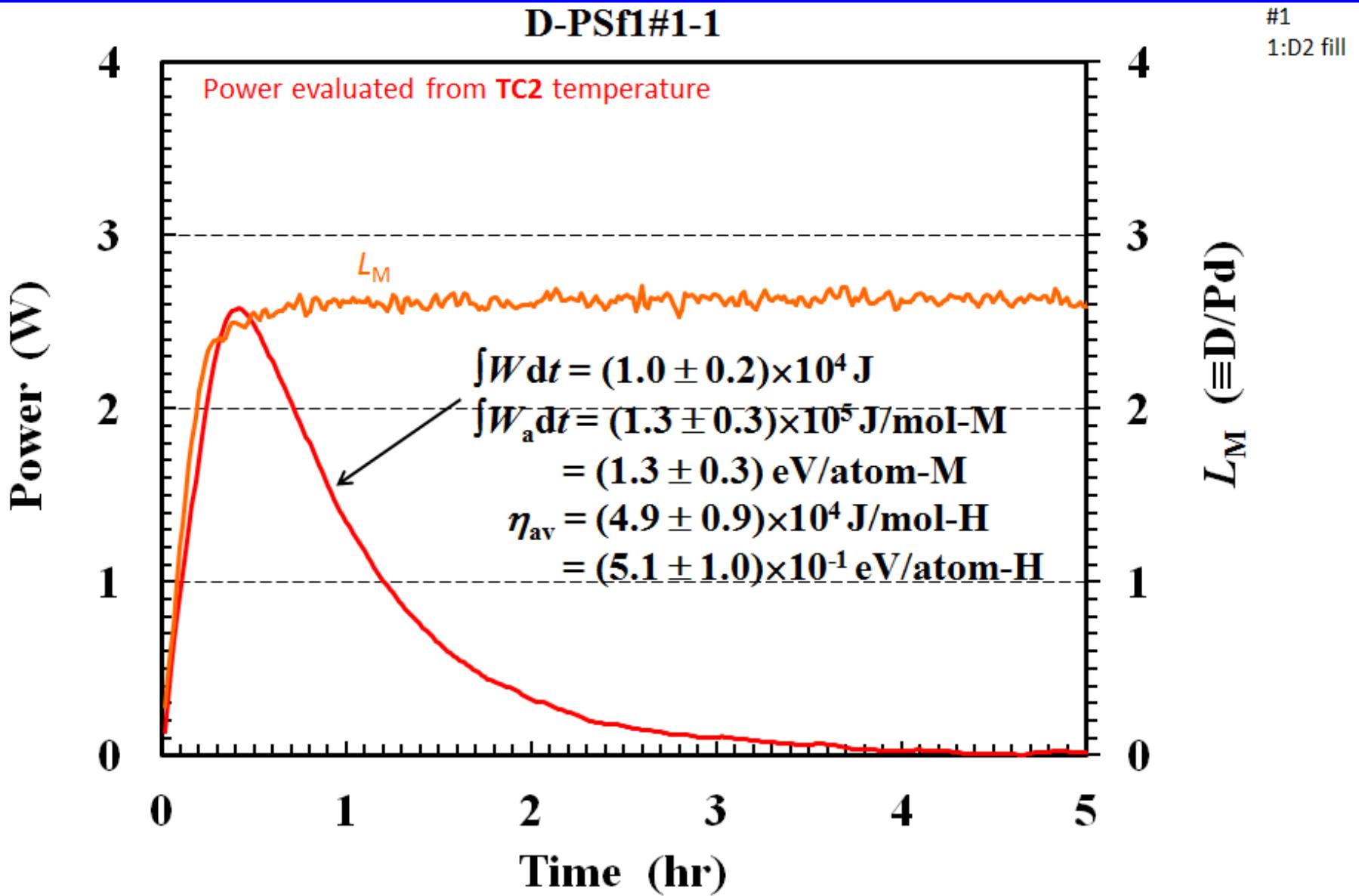
# Conversion of temperature to power produced in RC: Calibration (control sample: mp-silica) H-S2#1



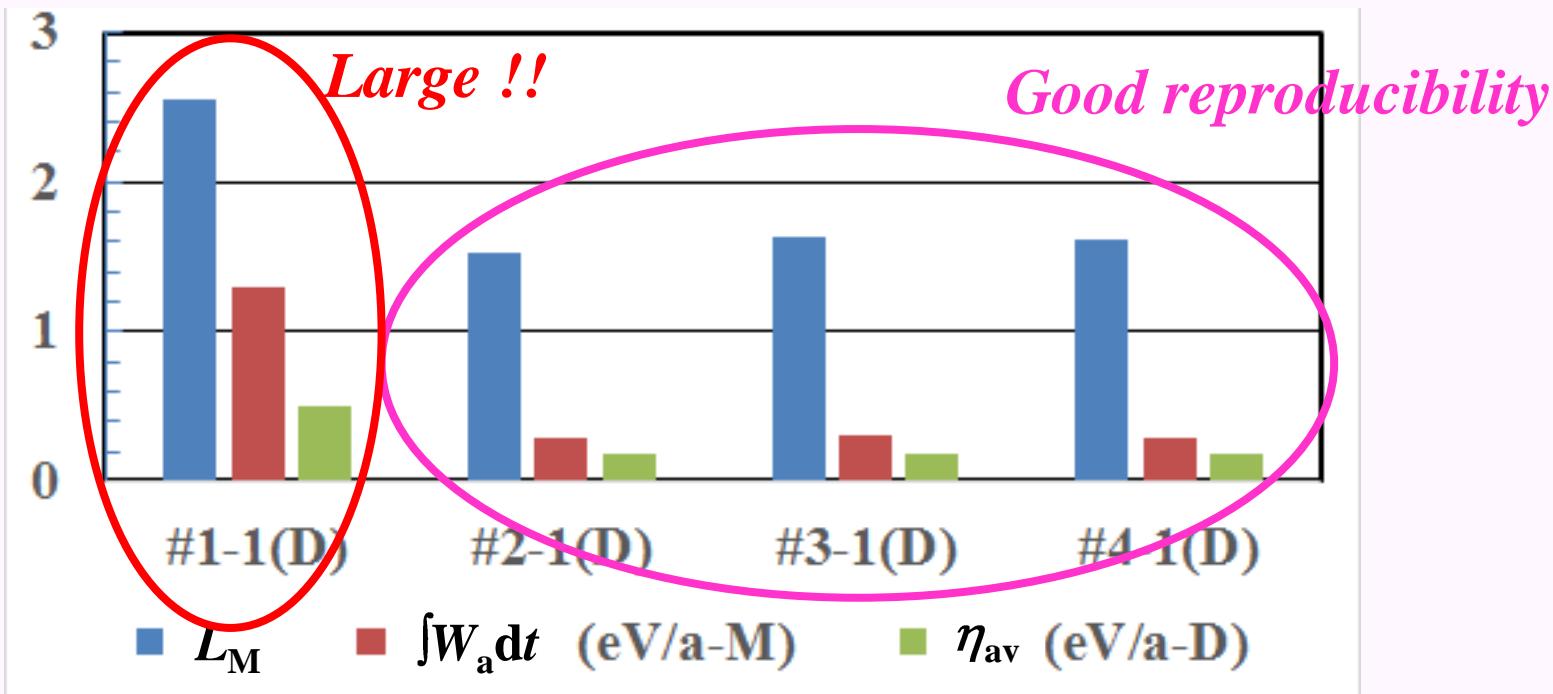
# Variation of deuterium-loading ratios, $L_M \equiv D/M$ ( $M=Pd$ ), in PSf1



# Emerging power and integrated heat under D<sub>2</sub> exposure of virgin PSf1 at room temperature (R.T.), and evolution of D-loading ratio L<sub>M</sub>



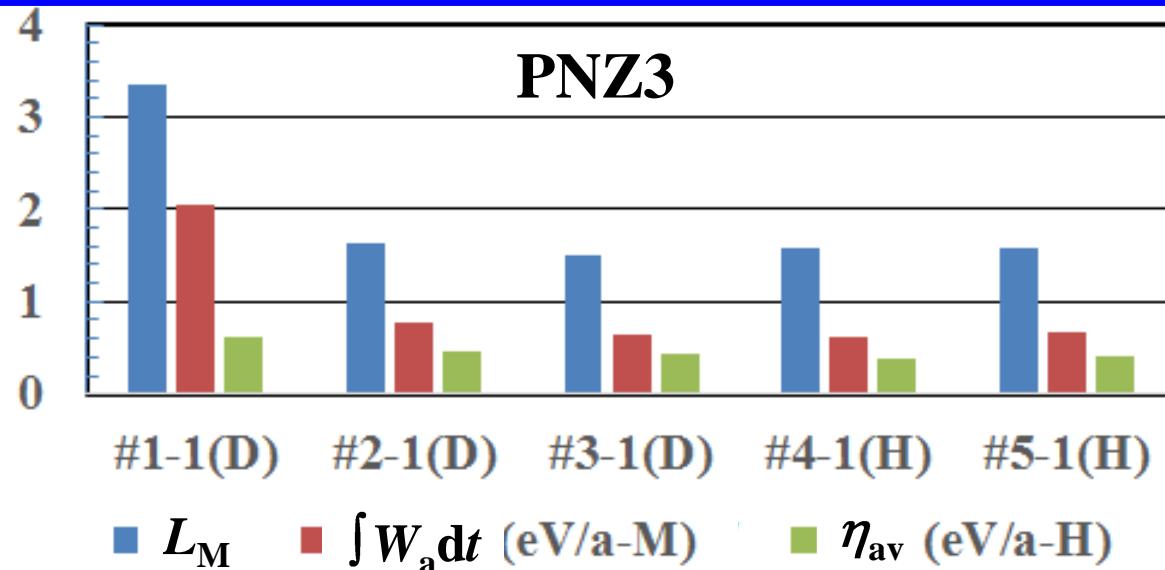
# Thermal energy output and D-loading ratio in R.T. phases, PSf1#n-1



		#1-1(D)	#2-1(D)	#3-1(D)	#4-1(D)
$L_M$	"M"=Pd	2.55E+00	1.53E+00	1.63E+00	1.61E+00
$E_a (\equiv \int W_a dt)$ (eV/a-M)		1.3E+00	2.9E-01	3.1E-01	2.9E-01
$\eta_{av}$ (eV/a-D)		5.1E-01	1.9E-01	1.9E-01	1.8E-01

may be explainable by known chemical reactions.

# Thermal energy output and loading ratios in R.T. phases, PNZ3#n-1



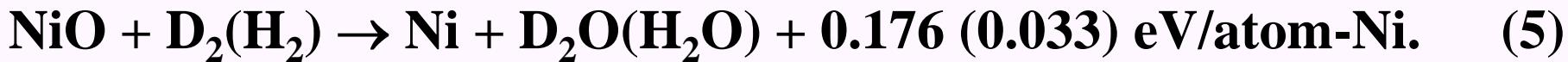
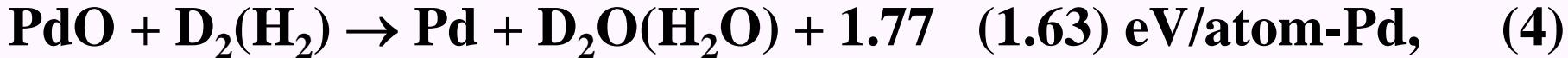
	PNZ3	#1-1(D)	#2-1(D)	#3-1(D)	#4-1(H)	#5-1(H)
$L_M$	"M"=Pd·Ni	3.35E+00	1.64E+00	1.50E+00	1.59E+00	1.57E+00
$E_a \equiv \int W_a dt$ (eV/a-M)		2.04E+00	7.68E-01	6.48E-01	6.17E-01	6.63E-01
$\eta_{av}$	(eV/a-H)		6.09E-01	4.67E-01	4.32E-01	3.89E-01

Very large  
 $L_M, E_a, \eta_{av}$

Ni absorbs at R.T.  
(Catalytic effect of Pd)

Fairly large  $L_M, E_a, \eta_{av}$ :  
 $\text{NiZrD}_{2.5} \leftrightarrow \text{ZrNi} + \text{D}_2$

# Plausible chemistry for D(H)-absorption and energy release in PNZ samples at R.T.: Existence of NiZr<sub>2</sub> phase may be the key.



( $L_M(=H/Ni)=4.5$ )

(2.85 eV/a-Ni) = (0.63 eV/a-H)

(: *Main reaction in #1-1?*)

*reversible*)

(*Reaction in #n-1 (n≥2) ?:*

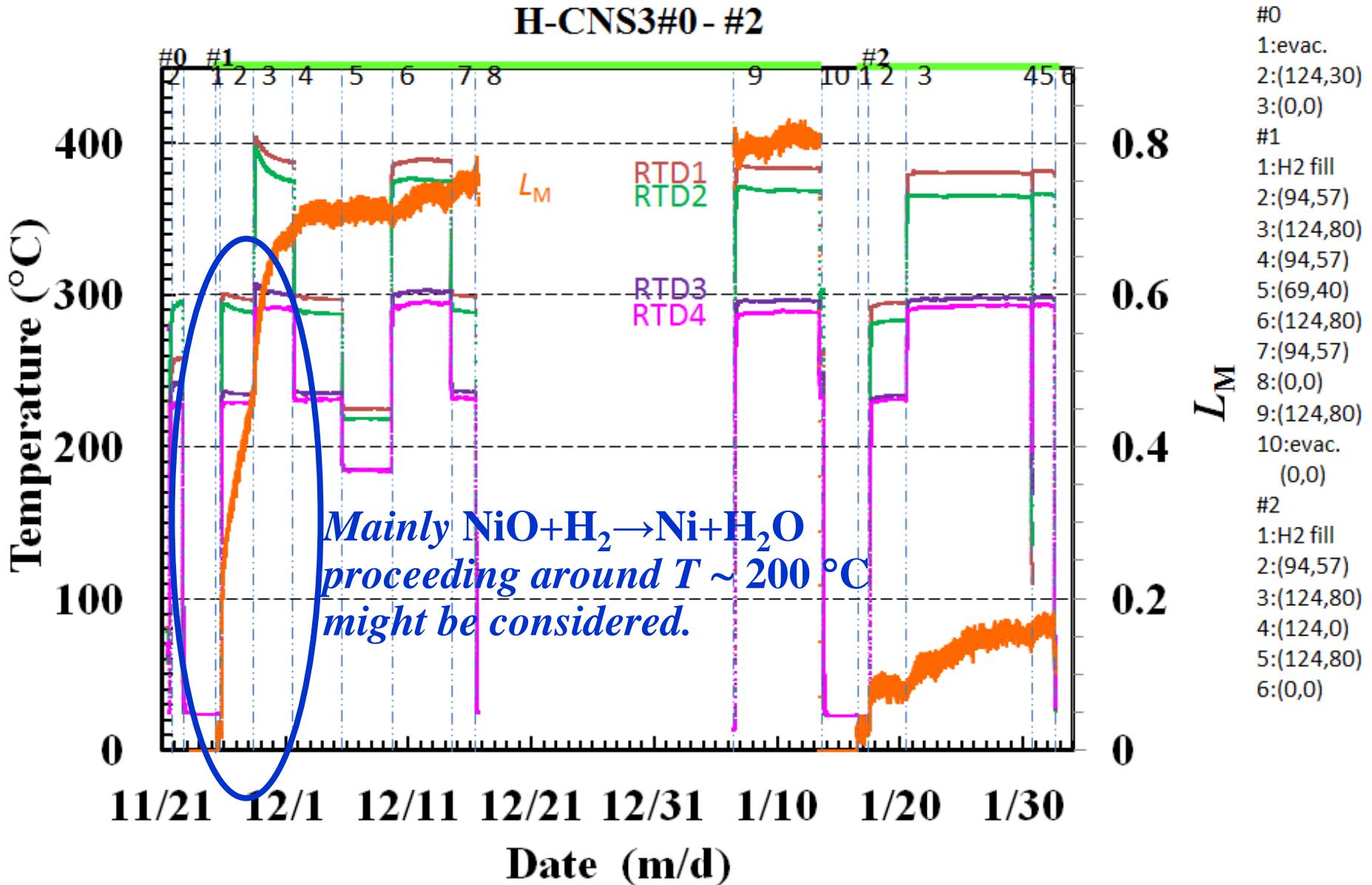


(*After re-calcination in air*)

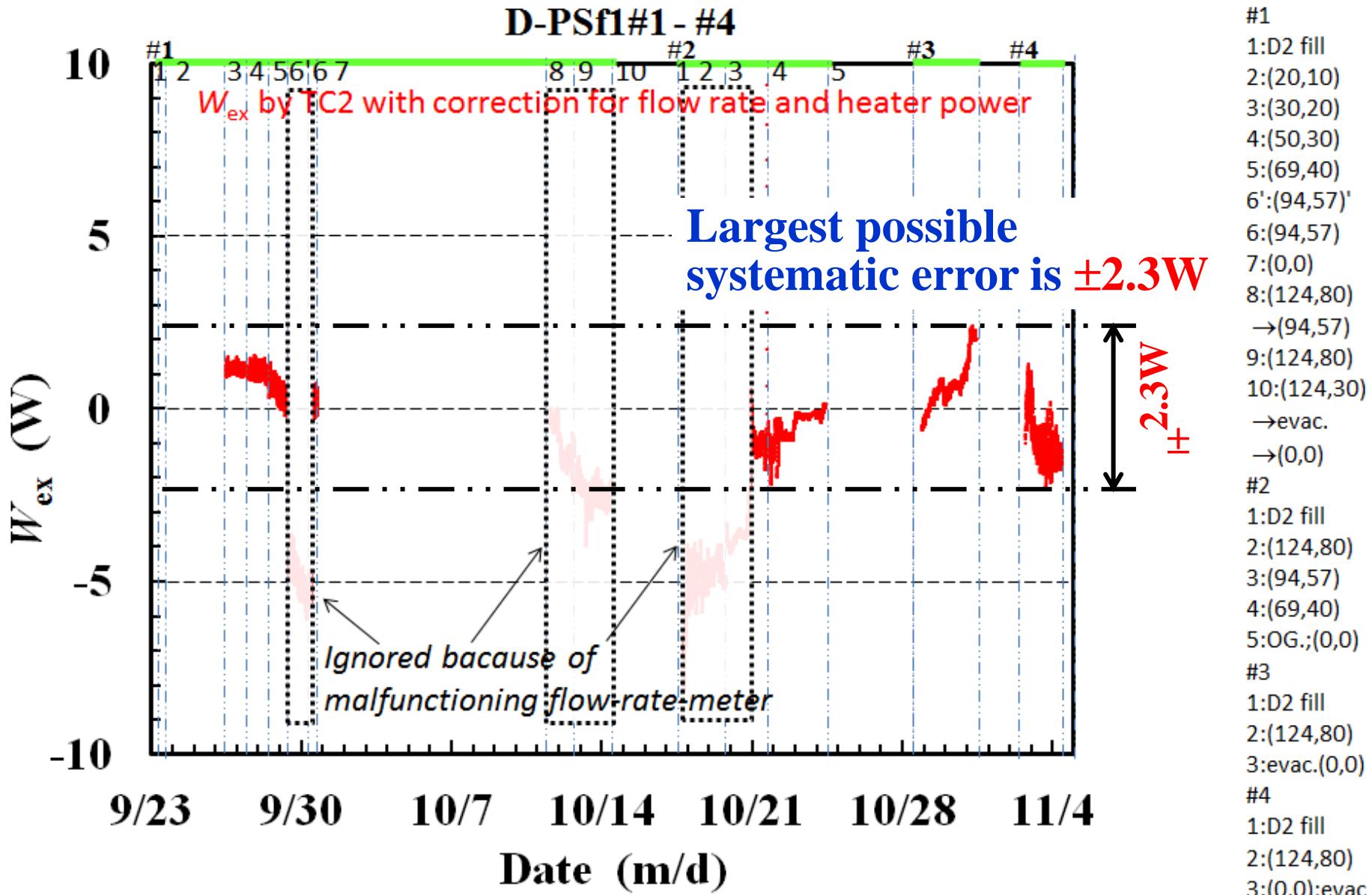


\* P. Dantzer, W. Luo, Ted B. Flanagan and J.d. Clewley; Calorimetrically Measured Enthalpies for the Reaction of H<sub>2</sub> (g) with Zr and Zr Alloys; Metallurgical Transactions A, **24A** (1993) 1471-1479.

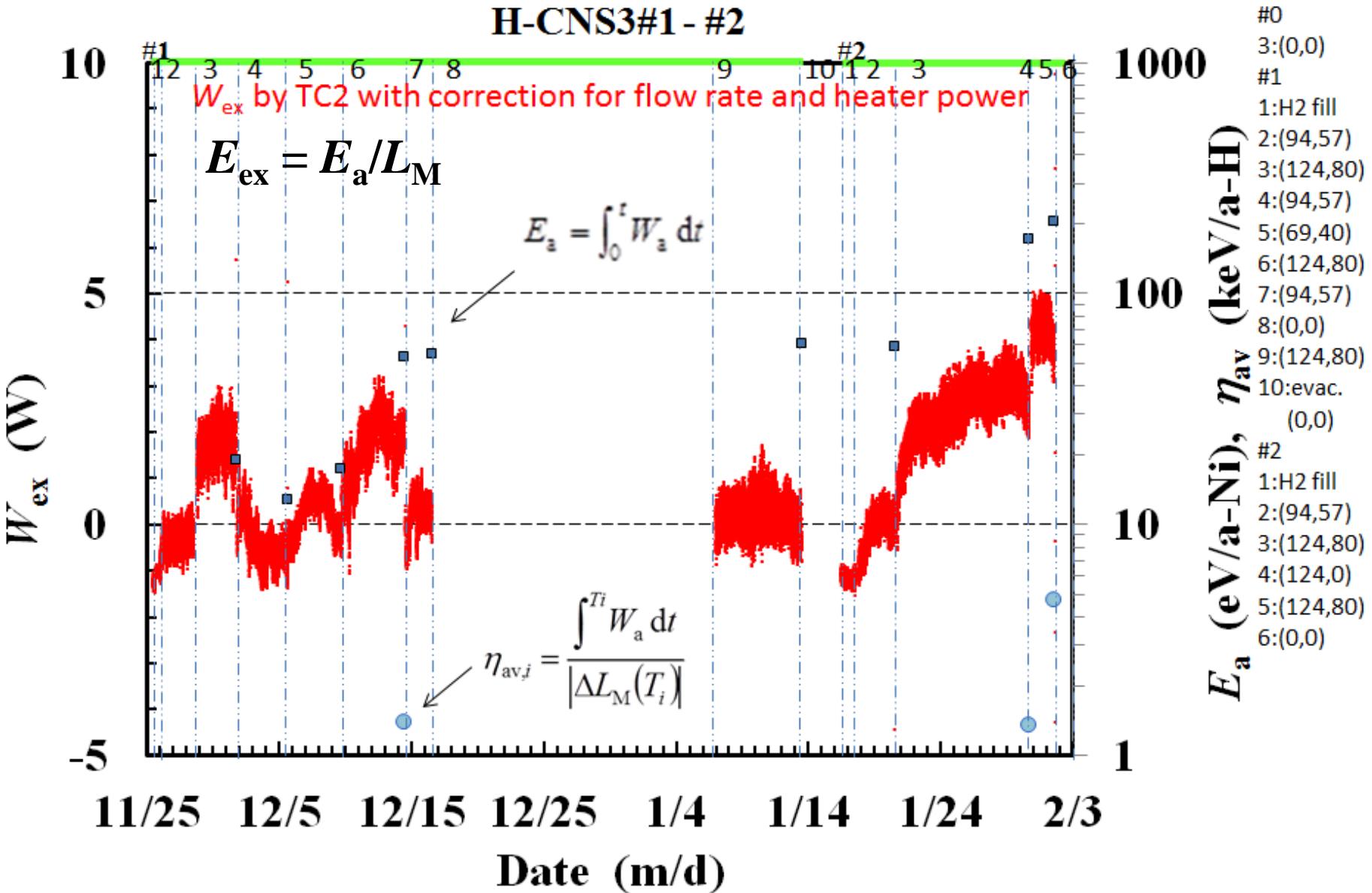
# Hydrogen absorption/consumption of CNS3 ( $L_M \equiv H/Pd$ )



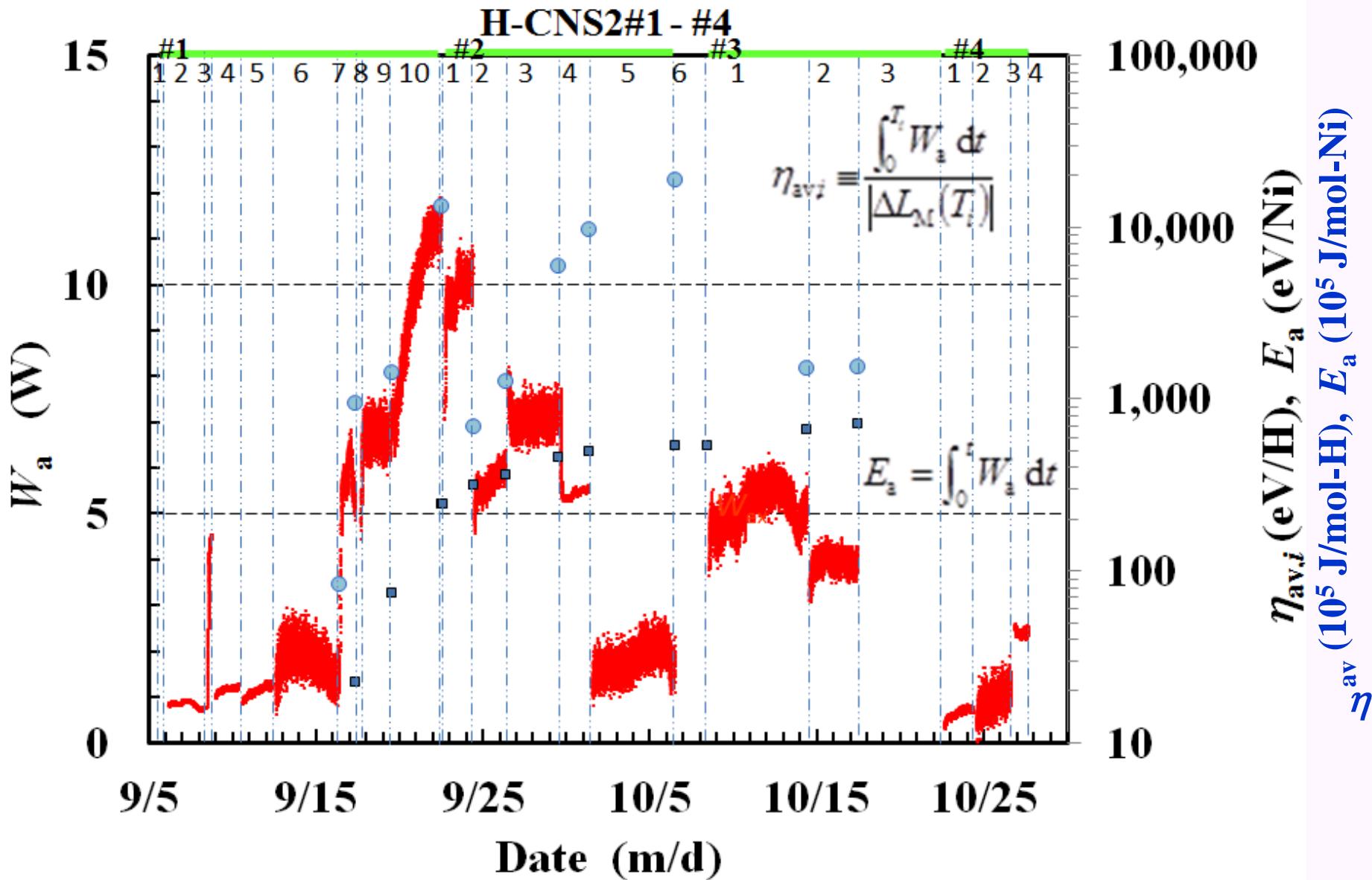
# Excess power ( $T_{\text{C2;PSf1}} - T_{\text{C2;mp-S}}$ ) at elevated temp.: No excess for PSf1



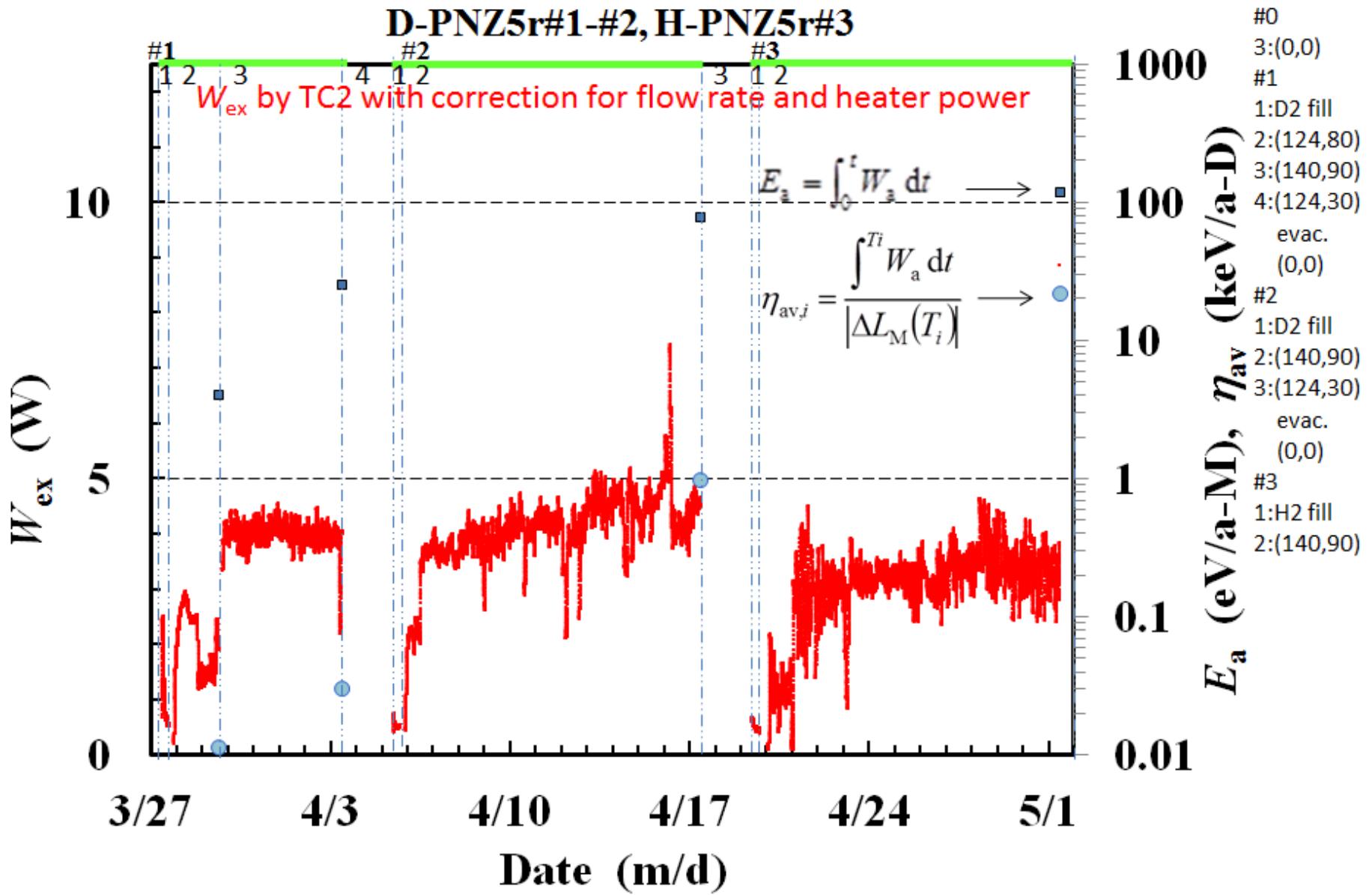
# Excess power for CNS3: 4.5 W with $E_{\text{ex}} \equiv E_a/L_M \sim 90 \text{ MJ/mol-H}$ .



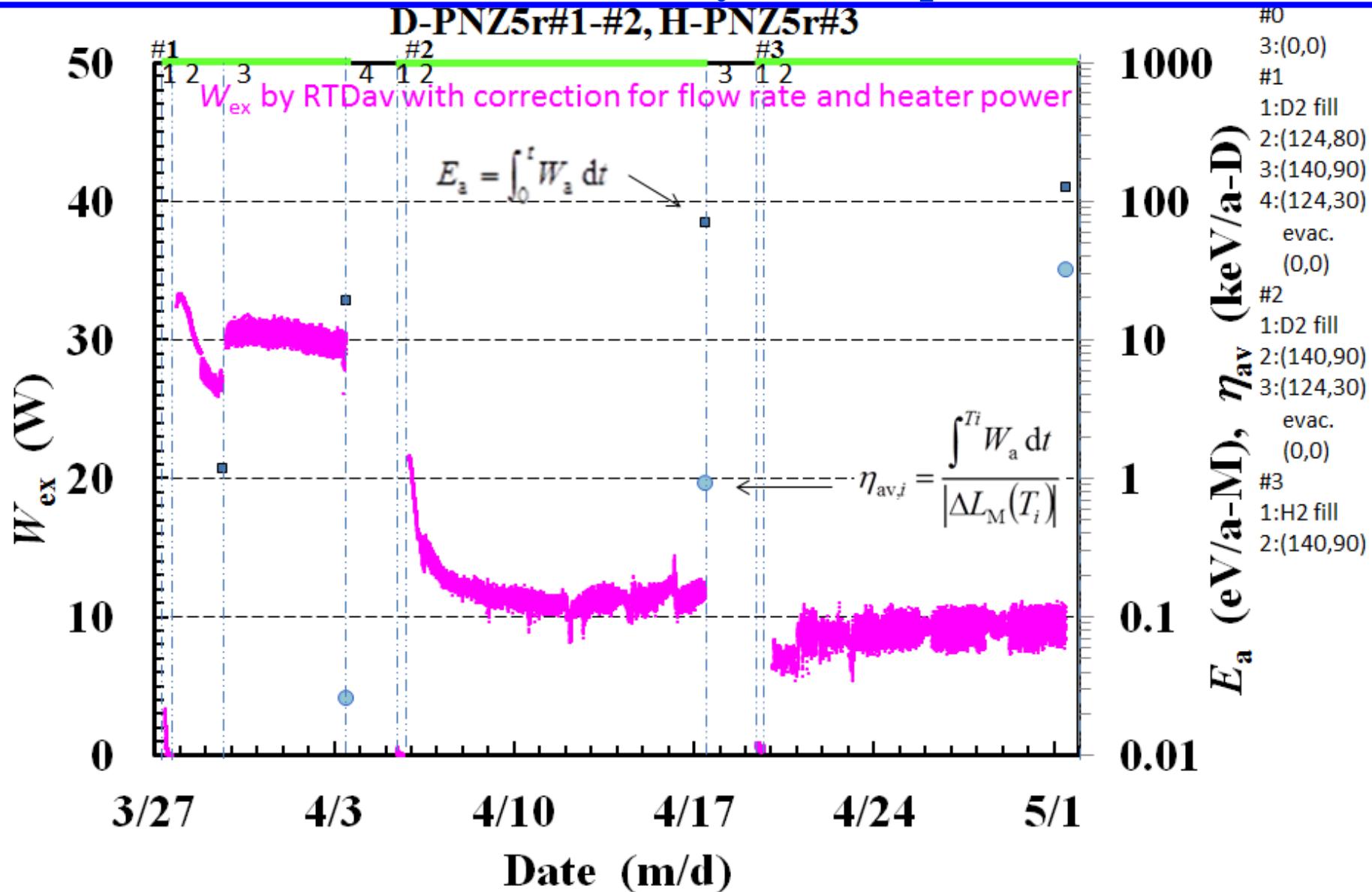
# Excess power is reproducible; 11 W for CNS2 with $E_{\text{ex}}$ 190 MJ/mol-H.



# Excess power evolution for PNZ5r: 4 ~ 5W with $E_{\text{ex}} \sim 9 \text{ MJ/mol-D}$



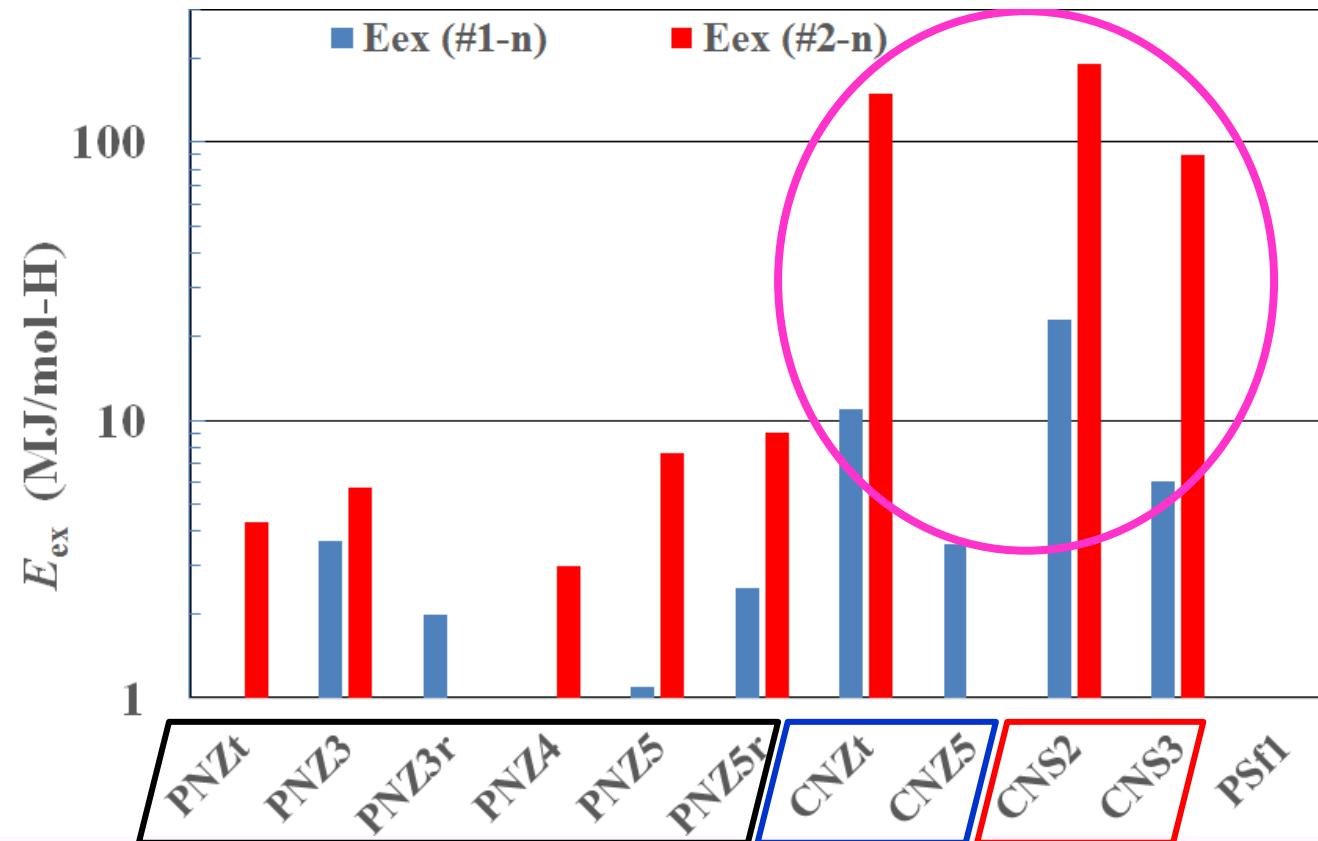
# Excess power for PNZ5r calculated with RTDav : Uniformization is one of the keys for the power enhancement.



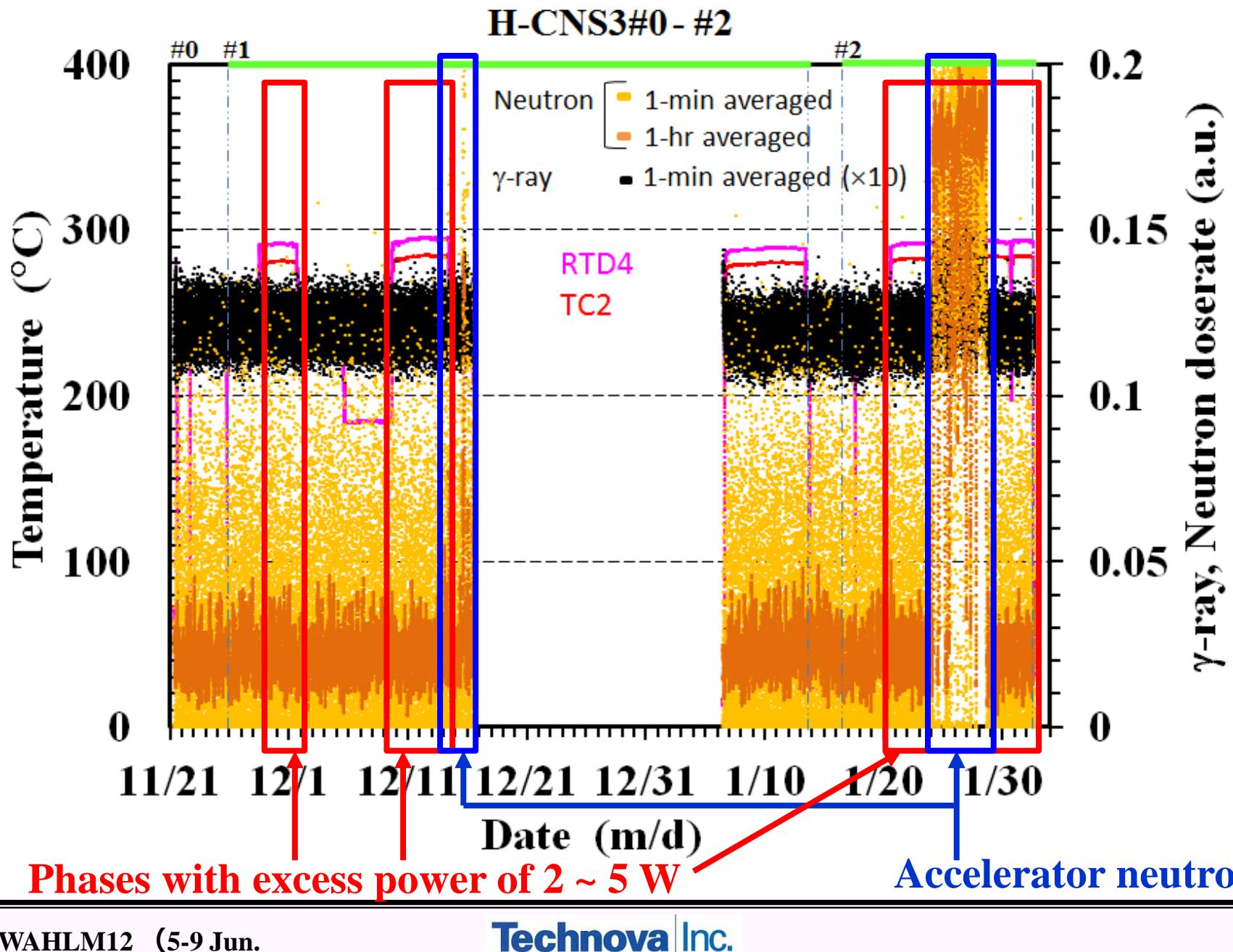
# Comparison of integrated excess heat at elevated temperatures

It appears that;

- CuNi is better than PdNi as the binary metal nanocomposites.
- ZrO<sub>2</sub> is better than SiO<sub>2</sub> as the supporter material, when compared in terms of excess energy per unit sample mass. (c.f. mass of CNZt is 54 g, while CNS3 150 g)



# Excess power accompanied by no hard radiations (neutrons and $\gamma$ rays)



# Summary of cooperative exp. at Kobe, 2016~2017

## ZrO<sub>2</sub>-supported

(a) Pd<sub>0.044</sub>Ni<sub>0.31</sub>Zr<sub>0.65</sub>; PNZ3, PNZ4, PNZ5

(b) Cu<sub>0.044</sub>Ni<sub>0.31</sub>Zr<sub>0.65</sub>; CNZ5

## SiO<sub>2</sub>-supported

(c) Cu<sub>0.008</sub>Ni<sub>0.079</sub> (mesoporous silica supported); CNS3

(d) Pd nanoparticles (mesoscopic SiO<sub>2</sub> supported); PSf1

- AHE at elevated temperatures **around 300 °C** were observed only for **binary**-metal nanoparticle samples ; no AHE for single-element-metal nanoparticles
- Observed both in D-Pd system and **H-Ni** system
- Excess power of **3 ~ 10 W** for weeks at 200 ~ 300 °C
- Integrated released energy of **3 ~ 30 MJ/mol-Ni**, or **4 ~ 90 MJ/mol-H**
- **ZrO<sub>2</sub>** is advantageous as the supporter material, when compared in terms of excess energy per sample mass.
- Anyway, **unexplainable** by any known chemical reaction.

## Short-term tasks for further research

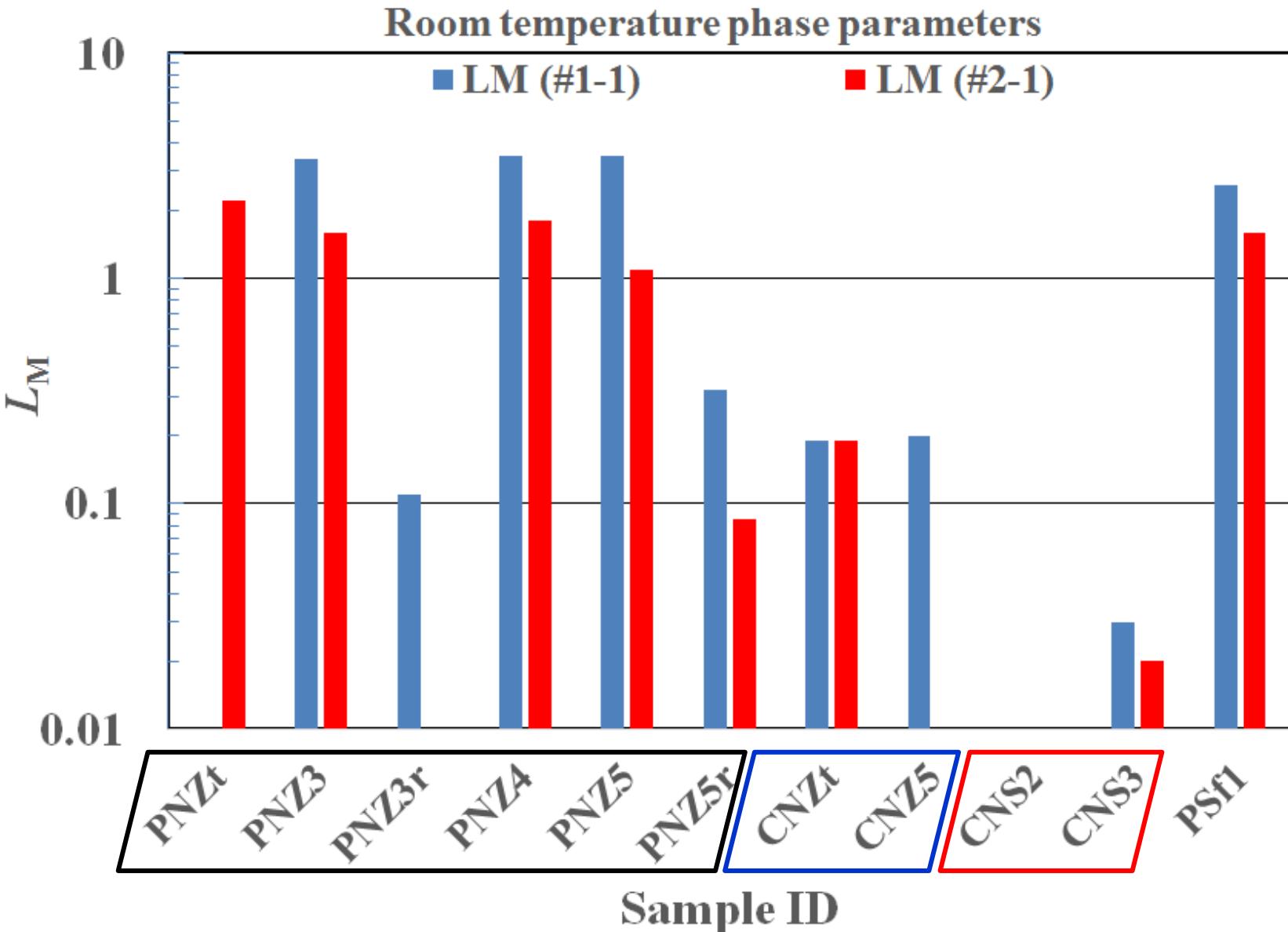
- (1) find optimum conditions (duration of calcination, particle size, etc.) for making binary metal nano-fabricated samples
- (2) make temperature distribution in RC uniform
- (3) find optimum molar ratio for binary samples
- (4) find optimum combination of the metal elements for binary samples
- (5) establish a scaling law of the output power
- (6) examine effectivity of ternary nanocomposites
- (7) design and make a prototype reactor with 1-kW output power

# **Supplement**

# Summary of the results in the past 3 years

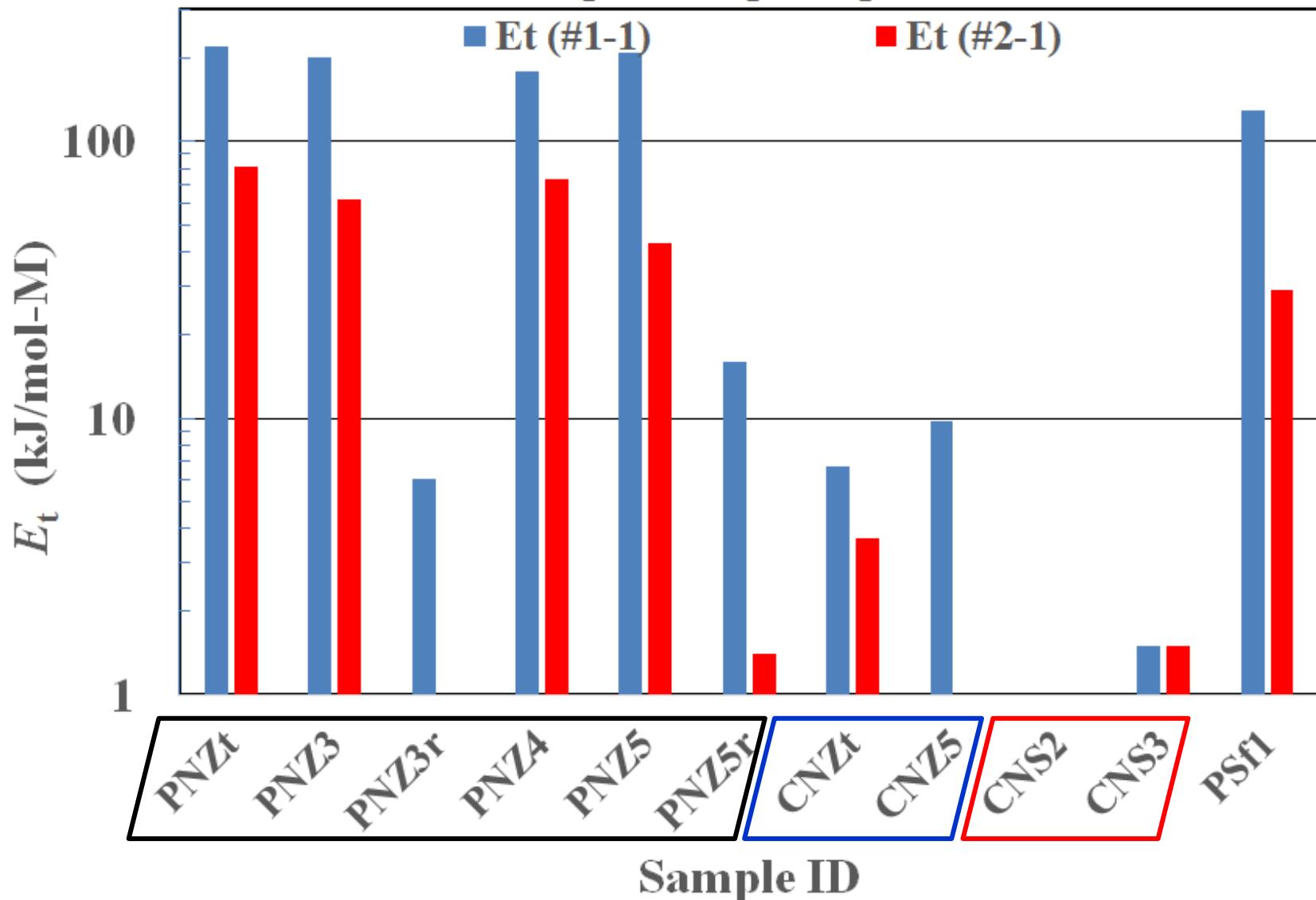
Sample ID	M(Ni or Pd) content	H (D or H)	RT				ET (> 250°C)						Remarks			
			L <sub>M</sub>		E <sub>t</sub> ≡ ∫W dt	η <sub>av</sub>	L <sub>M</sub>		W	η <sub>av</sub>		E <sub>ex</sub> ≡ ∫W dt / L <sub>M</sub>	RC	ref	α	
	(g)				(kJ/m-M)	(eV/H)			(W)	(keV/H)		(MJ/m-H)	old /new	fitting func	variable	
(NEDO)			#1	#2	#1	#2	#1	#2	#1	#2	#1	#2	#1	#2	#1	#2
PNZt	6.4	D(H)	(1.1)	2.2	220	81	(2.1)	0.39	1.5	0.15	5.9	2.6	(0.29)	0.77	(7.8)	4.3
PNZ3	20.0	D	3.4	1.6	200	62	0.61	0.43	2.8	1.1	8.0	10	6.5	16	3.7	5.7
PNZ3r	18.8	H	0.11	(5.3)	6.0	0	0.62	0	2.1	(7.4)	8.0	---	0.19	---	2.0	---
PNZ4	23.0	D	3.5	1.8	180	73	0.56	0.43	3.1	1.1	---	4.5	---	4.4	---	3.0
PNZ5	41.1	D	3.5	1.1	210	43	0.63	0.4	3.1	0.55	3.5	4.2	0.4	1.3	1.1	7.6
PNZ5r	40.7	D	0.32	0.085	16	1.4	0.53	0.17	0.7	0.2	3.7	4.5	0.025	1.0	2.5	9.0
CNZt	9.1	H(D)	0.19	0.19	6.7	3.7	0.37	0.2	1.7	0.2	4.0	2.2	1.7	0.83	11	150
CNZ5	22.0	H	0.2	---	9.8	---	0.5	---	1.9	---	3.3	---	3.4	---	3.6	---
CNS2	12.1	H	0.01	---	0	---	0	---	1.1	0.15	11	7.2	11	20	23	190
CNS3	11.4	H	0.03	0.02	1.5	1.5	0.57	0.65	0.8	0.16	2.4	4.4	1.4	4.7	6.0	90
PSf1	8.4	D	2.6	1.6	130	29	0.51	0.19	1.6	0.7	<1	<2.2	0	0	0	0

# Loading ratio $L_M$ at R.T.

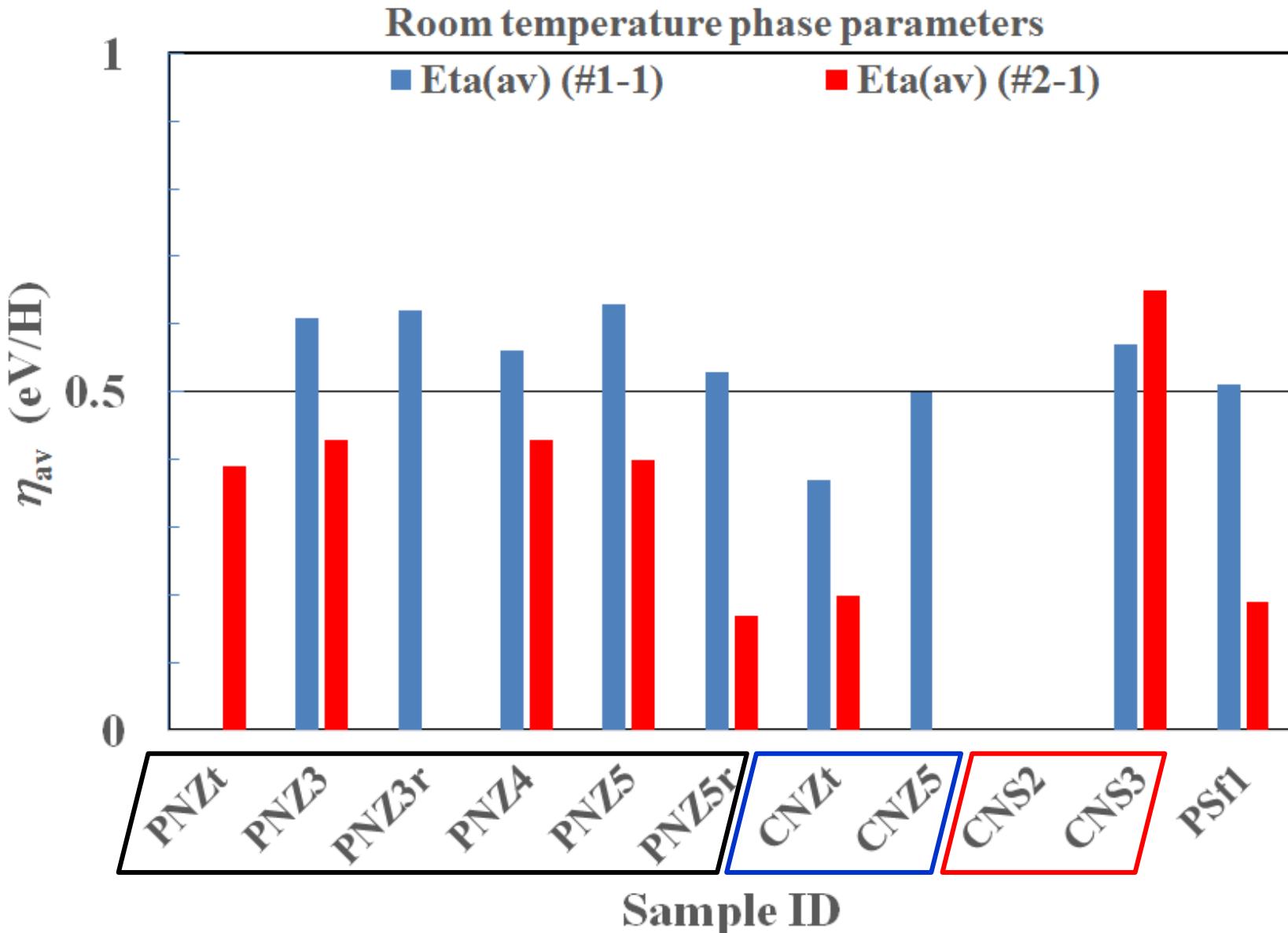


# Absorption energy $E_t$ at R.T.

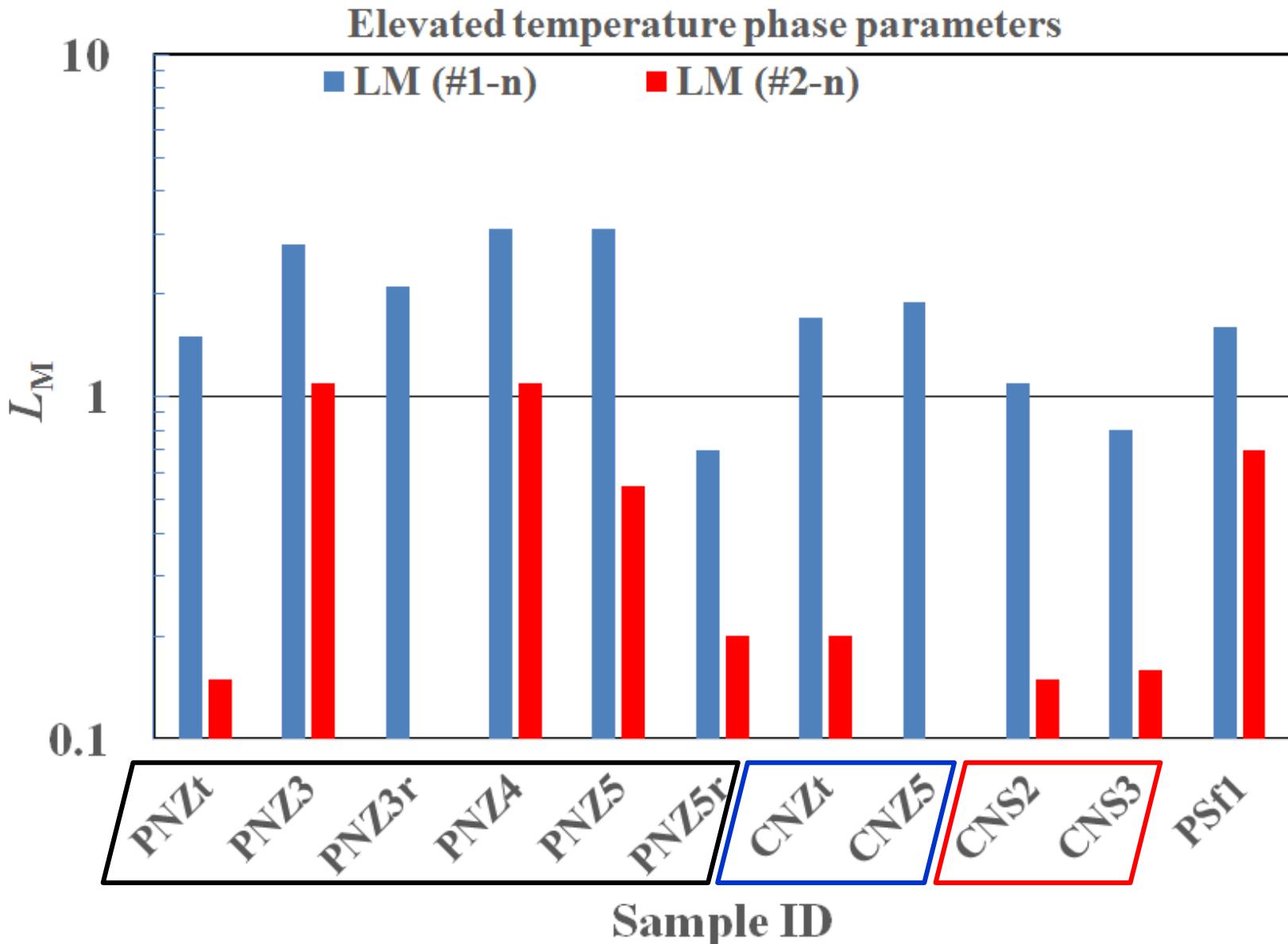
Room temperature phase parameters



# Specific absorption energy $\eta_{av}$ at R.T.

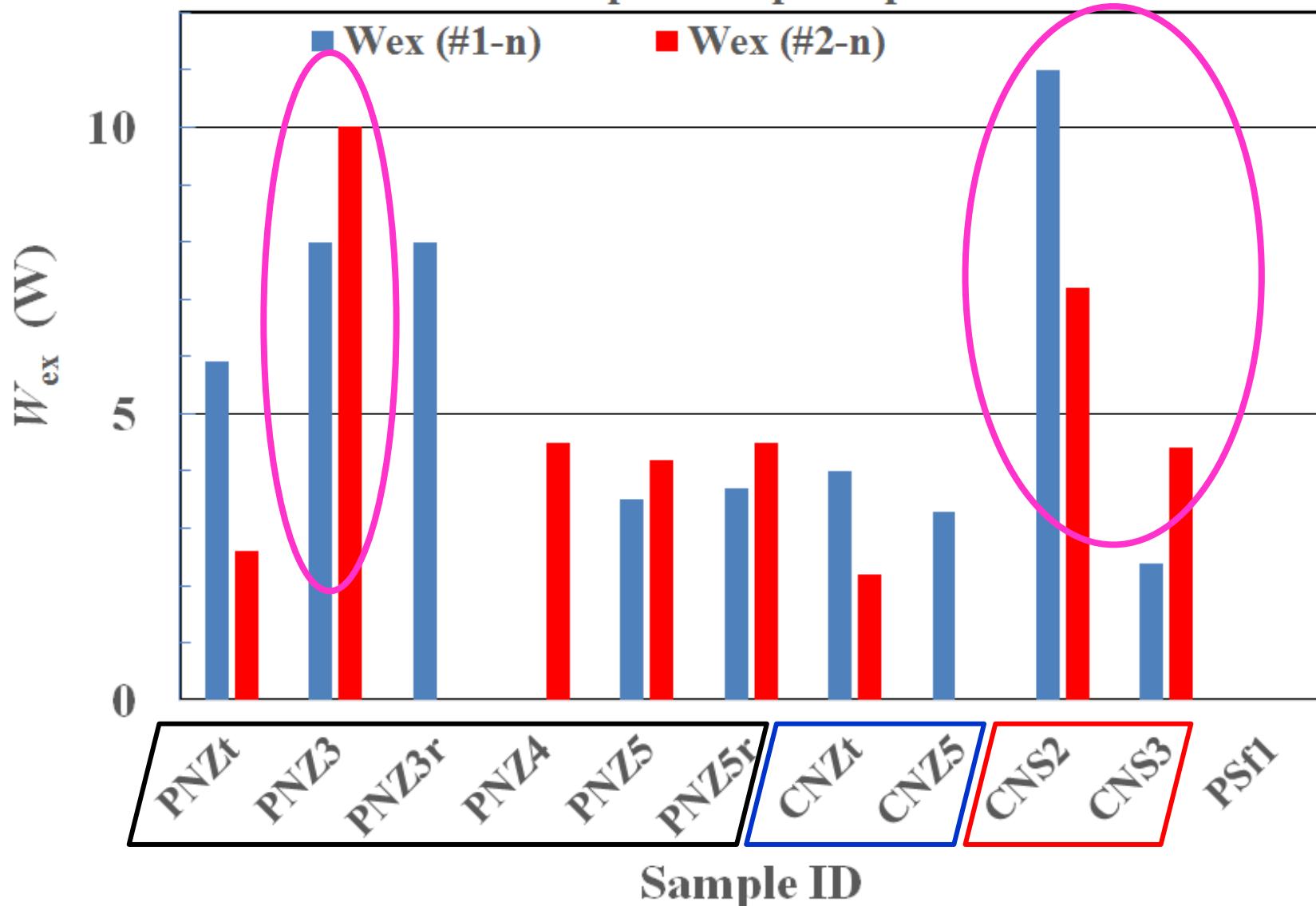


# Loading ratio $L_M$ at E.T.



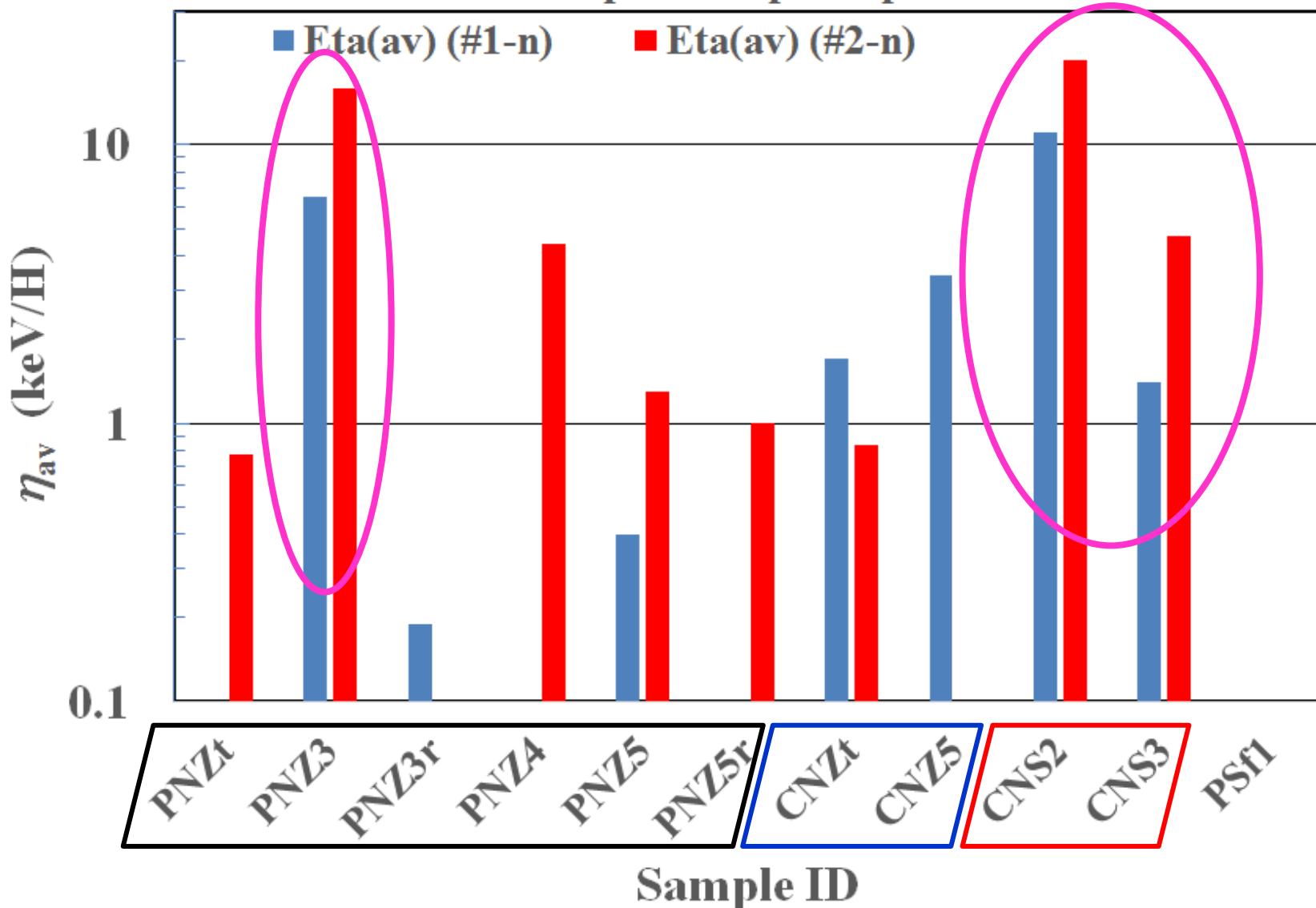
# Excess power $W_{\text{ex}}$ at E.T.

Elevated temperature phase parameters



# Specific sorption energy $\eta_{av}$ at E.T.

Elevated temperature phase parameters



# Earlier results by Technova-Kobe group

- Proc. ICCF14 (2011) 400-408  
Proc. JCF9 (2009) 23-28/ ibid. 29-35  
Proc. ICCF15 (2011) 216-220/ ibid. 94-99/ ibid. 297-302  
**Phys. Lett. A 373** (2009) 3109–3112  
**J. Condensed Matter Nucl. Sci. 4** (2011) 56-68  
Proc. JCF10 (2010) 14-19/ ibid. 20-25/ ibid. 46-53  
**LENR-NET SB 3** (2010) ACS  
**J. Condensed Matter Nucl. Sci. 5** (2011) 42-51/ ibid. 17-33  
Proc. JCF11 (2011) 10-15/ 16-22/ ibid. 47-52  
**J. Condensed Matter Nucl. Sci. 10** (2013) 46-62  
Proc. JCF12 (2012) 1-9/ ibid. 10-18  
**J. Condensed Matter Nucl. Sci. 13** (2014) 471–484/ ibid. 277-289  
Proc. JCF13 (2013) 214-229/ ibid. 230-241  
**J. Condensed Matter Nucl. Sci. 15** (2015) 23-32/ ibid. 231-239  
Proc. JCF14 (2014) 1-13  
Proc. JCF15 (2015) 1-19  
**Current Science, 108** (2015) 589-593  
**J. Condensed Matter Nucl. Sci. 19** (2015) 135-144  
Proc. JCF16 (2016) 135-144

## Equations used for correction for flow rate fluctuation

$$R_h = F^\alpha \cdot \rho \cdot C \cdot (T_{C2} - T_{C6}) / (W_1 + W_2), \quad (1)$$

$$\begin{aligned} \Delta T_{C2} &= (\frac{dT_{C2}}{dF}) \cdot \Delta F \\ &= (-\Delta F/F) \cdot (W_1 + W_2) \cdot (\frac{dT_{C2}}{dW}) \cdot \alpha. \end{aligned} \quad (2)$$

$$\alpha = 1.9 \times 10^{-2} \cdot \exp[4.0 \cdot (F/F_0)]. \quad (3)$$